

Towards feedback control of the cell-cycle across a population of yeast cells

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Abstract—Cells are defined by their unique ability to self-replicate through cell division. This periodic process is known as the cell-cycle and it happens with a defined period in each cell. The budding yeast divides asymmetrically with a mother cell generating multiple daughter cells. Within the cell population each cell divides with the same period but asynchronously. Here, we investigate the problem of synchronising the cell-cycle across a population of yeast cells through a microfluidics-based feedback control platform. We propose a theoretical and experimental approach for cell-cycle control by considering a yeast strain that can be forced to start the cell-cycle by changing growth medium. The duration of the cell-cycle is strictly linked to the cell volume growth, hence a hard constraint in the controller design is to prevent excessive volume growth. We experimentally characterised the yeast strain and derived a simplified phase-oscillator model of the cell-cycle. We then designed and implemented three impulsive control strategies to achieve maximal synchronisation across the population and assessed their control performance by numerical simulations. The first two controllers are based on event-triggered strategies, while the third uses a model predictive control (MPC) algorithm to select the sequence of control impulses while satisfying built-in constraints on volume growth. We compared the three strategies by computing two cost functions: one quantifying the level of synchronisation across the cell population and the other volume growth during the process. We demonstrated that the proposed control approaches can effectively achieve an acceptable trade-off between two conflicting control objectives: (i) obtaining maximal synchronisation of the cell cycle across the population while (ii) minimizing volume growth. The results can be used to implement effective strategies to unfold the biological mechanisms controlling cell cycle and volume growth in yeast cells.

I. INTRODUCTION

Attempts to apply engineering principles to biological processes to understand and build new functions in cells have led to a growing interdisciplinary research community blending Synthetic Biology with Control Engineering, aptly named Cybergenetics. Currently synthetic circuits can perform only very basic functions thus having a limited impact

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in biotechnology and biomedicine. Control engineering is a key discipline that provides the theoretical and methodological tools to engineer complex systems and make sure they behave in the desired way across a range of operating conditions. Application and adaption of established theories and techniques from conventional control engineering have been hampered by the peculiarities of biological systems, such as cell-to-cell variability, metabolic load, cross-talking and practical realizability [1].

Several studies have demonstrated the feasibility of using real-time feedback control approaches to drive simple cellular processes by means of optogenetics or microfluidics approaches [2]–[8], guaranteeing an accuracy that was hitherto unachievable. However, besides proof-of-concepts, the real potential of these approaches has not yet been thoroughly investigated.

Here, we investigate the feasibility of controlling a fundamental and complex mechanism present in each cell: the cell-cycle. This process can be seen as a biological oscillator characterised by a fixed period in each cell, but with different phases across cells. During the cell-cycle, the cell progresses in a sequential and unidirectional manner through different phases (growth, DNA synthesis, mitosis) to make a copy of itself. The control objective we want to achieve is to synchronise the cell cycle across the cell population, thus having all yeast cells budding at the same time. All the available methods in yeast biology do not really “synchronise” the cell population, at least according to the terminology of dynamical system theory, but rather just force each cell in the population to start from the same initial condition. Previous studies addressed the synchronisation problem by considering only an open-loop control strategy where an external periodic input was used to entrain the population of yeast cells, with limited success [9]. Here, we consider the implementation of a feedback control strategy based on an *external* control approach where a computer interfaced with living cells steers their dynamics by means of microfluidics whereas a microscope measures the cells’ output.

We first derived a simplified phase-oscillator model of cell-cycle motivated by previous work [9], whose parameters were fitted from experimental data. We used this model both for numerical simulations and for designing control strategies. We designed, numerically simulated and compared three different control strategies, two of which are based on input-output control and one on a model predictive control (MPC) strategy.

We then compared the three strategies against three performance indices that take into account the level of syn-

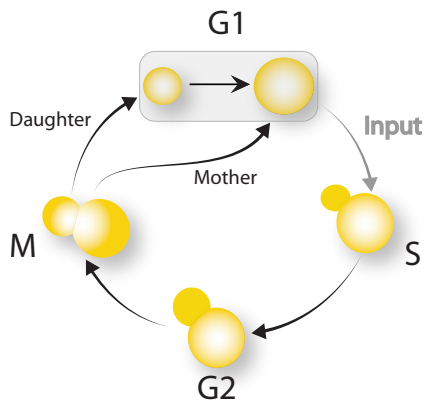


Fig. 1. Cell cycle process in a budding yeast manipulated genetically to halt the cell cycle in the G1 phase, unless an external stimulus is provided [10].

chronisation across the cell population quantified through the Kuramoto's order parameter and the cell volume growth during the process.

Our results show the feasibility of applying feedback control strategy to steer a complex biological process such as the cell-cycle and can be instrumental for their implementation in-vivo.

II. DESCRIPTION OF THE BIOLOGICAL SYSTEM AND CHARACTERISATION

To address the cell-cycle synchronisation problem, we chose a budding yeast strain whose cell-cycle (shown in Figure 1) can be halted at the G1 phase in the presence of methionine, or allowed to progress to the S phase in the absence of methionine [10].

A. Biological system

In the chosen yeast strain, all the endogenous genes encoding the G1 cyclins (*CLN1*, *CLN2* and *CLN3*) are deleted, thus making the cells unable to progress towards the S phase. To enable control of the cycle progression by changing growth medium, the endogenous *CLN2* gene was inserted downstream of the methionine repressible promoter *P_{MET3}*. In this way, the cell-cycle can progress to the S phase only in the absence of methionine. To track the cell-cycle progression, a yellow fluorescent protein (YFP) was inserted downstream of the endogenous *CLN2* promoter. Since the *CLN2* promoter is activated in G1 and repressed in G2, the yellow fluorescence reporter can be used as a proxy of the cell-cycle phase.

B. Experimental characterisation

We previously implemented a microfluidics experimental platform to enable real-time observation and control of gene expression in yeast cells [8], [11]. We employed this platform to perform a preliminary time-lapse experiment in which cells were grown in the absence of methionine for 18 hours, thus enabling them to cycle. We quantified at single-cell level the YFP fluorescence signal expressed by the endogenous *CLN2* promoter, as well as the area occupied by each cell

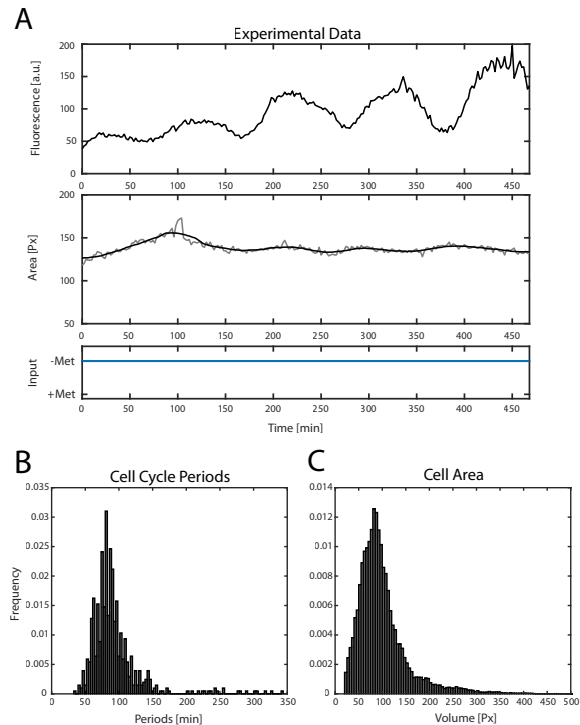


Fig. 2. Experimental characterisation of the biological system. (A) Experimental data of a single cell tracked for 500 min. The top panel shows the fluorescence signal measured by a fluorescence microscope at 2 min intervals. The middle panel shows the cell area in pixels. Cells were grown in the absence of methionine, as shown in the bottom panel. (B) Histogram of cell cycle duration across cells. (C) Histogram of cell area across cells.

in the field, as shown in Figure 2A. To reduce the effect of measurement noise, we applied a bandpass Butterworth filter to the fluorescence signals. The filter cut-off frequencies ($f_H = 5 \cdot 10^{-4}$ Hz and $f_L = 4 \cdot 10^{-5}$ Hz) are chosen in the range [30, 400] min, as the cell-cycle duration is biologically constrained within this interval.

The measured cell-cycle duration across cells (Figure 2B) can be approximated by a normal distribution $\mathcal{N}(\mu, \sigma^2)$ with mean $\mu = 84.47$ min and standard deviation $\sigma = 19.33$ min. As expected, the mean value μ is in line with previous observations [10]. We noted a high value for the standard deviation σ , which may be explained by the presence of cells in the field that are not cycling despite the activation of the endogenous gene *CLN2*. The estimated cell areas, which are proportional to the volume, are distributed as a log-normal distribution with mean $\mu = 4.48$ px and standard deviation $\sigma = 0.4$ px (Figure 2C).

C. Model derivation

To model the cell-cycle, we exploited the concept of phase reduction [12], [13]. We assumed that the cell-cycle can be described as a dynamical system of the general form:

$$\dot{x} = f(x, t), \quad (1)$$

where $x \in \mathbb{R}^n$ is the state vector and $t \in \mathbb{R}$ is time. If (1) has an exponentially stable limit cycle $\gamma \subset \mathbb{R}^n$ with period T_d ,

then (1) is an oscillator that, according the phase reduction method, can be modelled as a dynamical phase oscillator

$$\dot{\vartheta} = \omega, \quad (2)$$

where ϑ is the phase of the oscillator on the unit circle \mathbb{S}^1 and $\omega = \frac{2\pi}{T_d}$ is the angular frequency.

Let ϑ_c be the cell-cycle phase at budding, i.e. the phase at which the G1/S transition occurs. As the cell cycle is always in G1 in the presence of methionine, the phase dynamics can be described as:

$$\dot{\vartheta} = \begin{cases} 0 & \text{if } \vartheta \in [0, \vartheta_c[\\ \omega & \text{if } \vartheta \in [\vartheta_c, 2\pi[\end{cases}. \quad (3)$$

Thus, the phase linearly increases with rate ω only when the cell is in either S, G2 or M. As the cell-cycle is coupled to cell growth [9], we consider also cell volume dynamics. To this aim, we assume that a cell grows exponentially only during the G1 phase. Thus, the volume growth can be described as:

$$\dot{V} = \begin{cases} \beta V & \text{if } \vartheta \in [0, \vartheta_c[\\ 0 & \text{if } \vartheta \in [\vartheta_c, 2\pi[\end{cases}, \quad (4)$$

where $\beta > 0$ is the volume growth rate. We assume that cell division occurs at $\vartheta = 2\pi$. At each division event, the phase ϑ is reset to $\vartheta = 0$.

Let $u \in \{0, 1\}$ be the external trigger input to the system. We assume that, if $u = 1$, the cells are growing in the absence of methionine; conversely, if $u = 0$, they are growing in the presence of methionine. We then model the phase transition from G1 to S as the following reset condition:

$$\text{if } \vartheta \in [0, \vartheta_c[\wedge u = 1 \wedge V \geq V_c \implies \vartheta \mapsto \vartheta_c, \quad (5)$$

where V_c is the critical volume, defined as the minimum amount of volume needed to have the cell cycle progress towards the S phase.

III. PROBLEM STATEMENT

Let $N \in \mathbb{N}$ be the number of cells in the population. Consider each cell as an individual agent whose cell-cycle progression is mathematically described by the model composed by (3) and (4), together with the reset condition (5).

The control aim is to synchronise the cell-cycle across the cell population. As the duration of the cell-cycle is coupled to the volume growth, a desirable feature of the controller is to avoid excessive volume growth, which can be lethal for the cell.

Synchronisation in a population of oscillators can be quantified by means of the Kuramoto order parameter R [13] defined as the magnitude of the complex number

$$Z(t) := \frac{1}{N} \sum_{i=1}^N e^{j\vartheta_i(t)} = R(t) e^{j\Theta(t)}, \quad (6)$$

where ϑ_i is the phase of cell i . $R \in [0, 1]$ represents the mean phase coherence, an index to evaluate the synchronisation

among a population of oscillators. When R is equal to 1, all cells are synchronized onto the same phase.

Cell volume is quantified by measuring the average volume in the population:

$$\bar{V}(t) = \frac{1}{N} \sum_{k=1}^N V_i(t). \quad (7)$$

To evaluate the performance of the control algorithms, we introduce two cost functions:

$$J_R = 1 - \frac{1}{t_f} \int_0^{t_f} R^2(\tau) d\tau, \quad (8)$$

so that all cells are synchronized over the whole time interval when J_R is equal to zero; and:

$$J_V = \left(\frac{\bar{V}(t_f) - \bar{V}_0}{\bar{V}_{max} - \bar{V}_0} \right)^2, \quad (9)$$

with $J_V \in [0, 1]$, $\bar{V}_0 = \bar{V}(0)$ and $\bar{V}_{max} = \bar{V}_0 e^{\beta t_f}$. Here \bar{V}_{max} is the maximum value of the average volume that would be reached if all cells exponentially grew for all $t \in [0, t_f]$. Notice that volume growth is minimized over the time interval being considered if J_V is rendered as close as possible to 0.

The control problem can thus be stated as follows:

Problem 1: Given a population of N individual cells, which are described by (3), (4), (5), compute the control input u that minimises J_R and, possibly, J_V .

A. Numerical simulations

All in-silico simulations were performed using the Matlab `ode45` solver with event detection routines to accurately detect cell division at $\vartheta_i = 2\pi$ and the hitting of the critical volume $V_i = V_c$ for cells with initial volume $V_i < V_c$.

We considered a synthetic population consisting of $N = 100$ cells with random initial conditions. Specifically, the initial volumes $V_i(0)$ were drawn from the interval $[0.8 V_c, 1.2 V_c]$ and the initial phases $\vartheta_i(0)$ from the interval $[0, 2\pi[$, both with uniform distributions, and setting ϑ_i to 0 if $V_i < V_c$. Moreover we set $\vartheta_c = \frac{\pi}{4}$.

The volume growth rate is chosen as $\beta = 0.0083 [\text{a.u.}] \text{min}^{-1}$ and the critical volume as $V_c = 1000 [\text{a.u.}]$, following the same choice reported in [9].

Due to the high standard deviation in the cell cycle periods T_i identified from the experimental data, we considered also an additional case with a lower standard deviation (hence a lower value of the coefficient of variation $CV = \sigma/\mu$, where μ is the nominal cell cycle period T). Specifically:

- High variability case ($CV = 22.88\%$): T_i drawn from the normal distribution with parameters $\mu = 84.47$ min and $\sigma = 19.33$ min, winsorizing samples outside $[40, 138]$ min.
- Low variability case ($CV = 10\%$): T_i drawn from the normal distribution with parameters $\mu = 84.47$ min and $\sigma = 8.447$ min, winsorizing samples outside $[67, 101]$ min.

All simulations were stopped at $t_f = 6T$.

IV. CONTROL ALGORITHMS

We designed three control algorithms to solve Problem 1, that is to achieve the synchronisation of the yeast cell cycle, and concurrently the minimisation of the volume growth in heterogeneous populations of cells. The first control algorithm we present, named *Stop&Go control*, is trivial and hence it is used as benchmark to assess the performance of the other two more advanced control algorithms. The second control algorithm, that we named *Threshold control*, is an empirical control strategy. The third control algorithm is a *model predictive control* (MPC), which is widely exploited for external in-silico control of biological systems [6]–[8], [14].

A. Stop&Go control

The Stop&Go control algorithm consists into applying a control trigger $u = 1$ every time *all* cells are at $\vartheta_i = 0$, that is they have stopped at the G1 phase:

$$u = \begin{cases} 1, & \text{if } \vartheta_i = 0, \text{ for all } i \\ 0, & \text{otherwise} \end{cases} \quad (10)$$

At steady-state, that is after the first trigger, the control signal $u(t)$ becomes periodic with period $T_u \approx \frac{3\pi/2}{\omega_{\min}}$, where ω_{\min} is the angular frequency of the slowest cell in the population. This algorithm does not attempt to minimise the cell volume growth. Figure 3(a) depicts the phase $\vartheta_i(t)$ and volume $V_i(t)$ normalised by the critical volume V_c of the cells in the population together with the control input generated by this algorithm. The time evolution of the mean phase coherence $R(t)$ and the normalised average population volume $\bar{V}(t)/V_c$ are reported in Figure 3(b) where they are averaged over 10 trials with random initial conditions.

B. Threshold control

The Threshold control algorithm is a heuristic control strategy where a trigger $u = 1$ is applied only when there are no cells with phase ϑ_i in a certain interval $\mathcal{I}(k)$, that is

$$u = \begin{cases} 1, & \text{if } \vartheta_i \notin \mathcal{I}(k), \text{ for all } i \\ 0, & \text{otherwise} \end{cases} \quad (11)$$

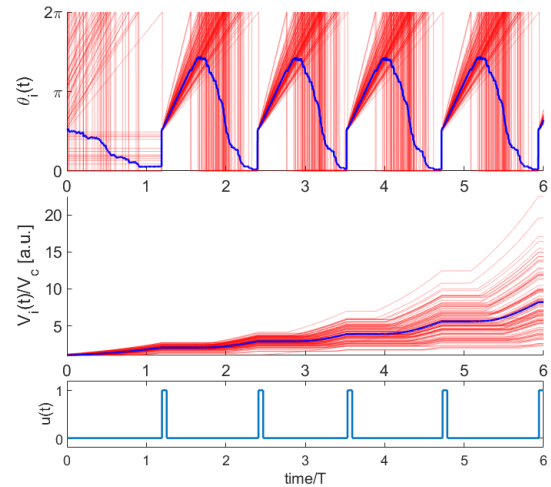
This interval is defined as

$$\mathcal{I}(k) := \left[\vartheta_c, \vartheta_c + \frac{3\pi}{4n}k \right],$$

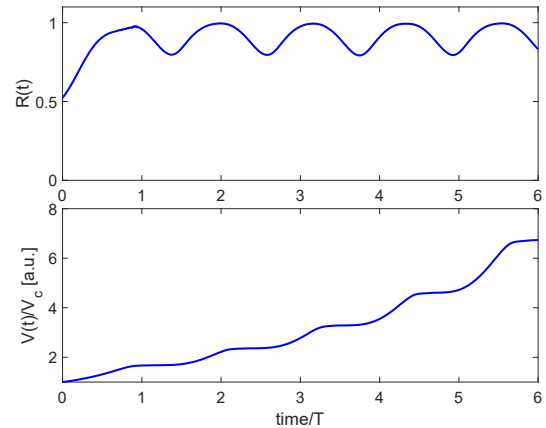
where n is the *first control parameter* and represents the number of sub-intervals in which the sector $[\vartheta_c, \vartheta_c + \frac{3\pi}{4}]$ is divided, as shown in blue in Figure 4. The right endpoint of the interval $\mathcal{I}(k)$ defines the *current threshold* $\vartheta_u(k) = \vartheta_c + \frac{3\pi}{4n}k$ whose values grows with $k \in \{1, \dots, n, 2n\}$. The evolution in time of k is defined as

$$k(t) = \begin{cases} \left\lceil \frac{t}{T_f} n \right\rceil, & \text{if } [t] \leq T_f \\ 2n, & \text{otherwise} \end{cases},$$

where $T_f < t_f$ is a *second control parameter* that represents the first time instant at which we want $k = 2n$. Therefore, at $t = T_f$ we have $\vartheta_u(2n) = 2\pi$, as $\vartheta_c = \frac{\pi}{4}$. Notice that when



(a) Time evolution of $\vartheta_i(t)$ and $\bar{V}_i(t)/V_c$, for one simulation trial, are reported in red colour. Their average values over the whole population are reported in blue. The corresponding control signal $u(t)$ generated by the Stop&Go algorithm is reported in the bottom panel.



(b) Time evolution of $R(t)$ and $\bar{V}(t)/V_c$ averaged over 10 simulation trials with random initial conditions.

Fig. 3. Stop&Go control: High-variability of T_i ($CV = 22.88\%$).

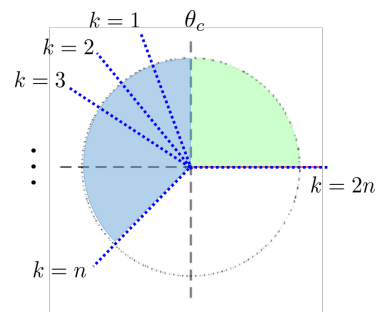


Fig. 4. Illustration of the evolution of the threshold ϑ_u in Threshold control algorithm. The phase interval $[\vartheta_c, \vartheta_c + \frac{3\pi}{4}]$ (depicted in blue) is divided into n equal subintervals. As $k(t)$ grows in time from 1 to $2n$, the interval $\mathcal{I}(k)$ with ϑ_u . The G1 phase is depicted in green, corresponding to the phase interval $[0, \vartheta_c]$. Cell phases are assumed to positively evolve in the anticlockwise direction.

this condition is met, the control laws (10) and (11) become equivalent and therefore this control algorithm behaves as the Stop&Go control.

Were the algorithm to be applied to a single cell, then the number of control triggers, say N_u over a certain time interval $[0, t_f]$ could be analytically computed as :

$$N_u(t_f) = \sum_{k=1}^n \left[\left(\omega \frac{T_f}{n} \right) / \left(\frac{3\pi}{4n} k \right) \right] + \left\lceil \frac{t_f - T_f}{T} \right\rceil.$$

However, due to the heterogeneity of cell-cycle duration across cells this number represents only an upper bound on the actual number of control triggers generated by the algorithm.

To limit volume growth (J_V), this algorithm is complemented with a time-dependent control. Specifically, even when the condition (11) on the phases is not satisfied, a control trigger is applied if the last trigger was applied more than $\left(\frac{3\pi k}{4n}\right)/\omega$ minutes ago, where ω is the nominal cell cycle angular frequency, that is $\omega = 2\pi/T$. This allows to avoid unnecessary volume growth due to wasted time waiting for “slow” cells to reach the current threshold $\vartheta_u(k)$.

Figure 5(a) shows the response of the cell population to the control input generated by the Threshold algorithm with control parameters $(n, T_f) = (8, 2T)$. The evolution of $R(t)$ and $\bar{V}(t)/V_c$ averaged over 10 simulation trials with random initial conditions and selected values of the control parameters (n, T_f) are reported in Figure 5(b).

C. Model Predictive Control

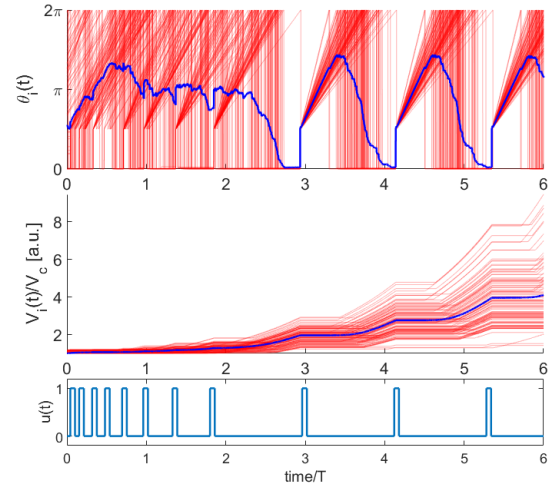
The MPC algorithm consists in solving an open-loop optimal control problem repeatedly over a receding horizon [15]. This means that at each iteration of the algorithm, the solution of the optimal open-loop control problem gives an optimal input that minimises a cost function over a finite prediction horizon T_p . The optimal input is applied over a finite control horizon $T_c \leq T_p$, hence discarding the remaining part of the computed optimal control action. Then, the optimisation is repeated again.

To address the problem of minimising the two conflicting performance indices J_R and J_V , we chose the cost function

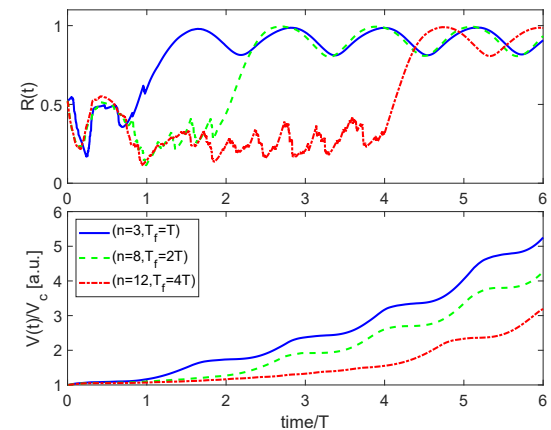
$$J = \alpha_R J_R + \alpha_V J_V, \quad (12)$$

which combines both J_R and J_V , defined in (8) and (9), with $t_f = T_p$, by assigning a different weight to each index function (*weighting method*) [16]. The choice of the weights α_R and α_V , with $\alpha_R \geq 0$, $\alpha_V \geq 0$, $\alpha_R + \alpha_V = 1$, affects the overall performance of the algorithm, hence they are considered as further control parameters, and represent a trade-off between the two different control objectives.

To reduce the computational complexity of the optimal control problem, the control input $u \in \mathcal{U}$ is assumed to be a finite sequence of triggers. Defining $P \in \mathbb{N}$ as the maximum number of triggers that may be applied in a finite prediction horizon, then the time interval occurring between two consecutive triggers is $\frac{T_p}{P}$. The feasible set \mathcal{U} is defined as the set of all admissible control sequences. Considering



(a) Time evolution of $\vartheta_i(t)$ and $\bar{V}_i(t)/V_c$, for one simulation trial, are reported in red. Average values over the whole population are reported in blue. The corresponding control signal $u(t)$ generated by the Threshold control algorithm with parameters $n = 8$, $T_f = 2T$ is reported in the bottom panel.

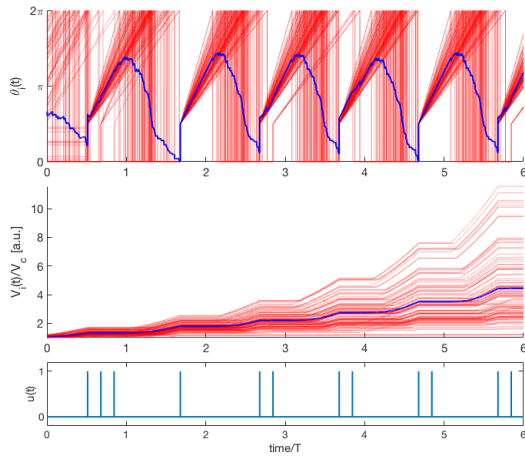


(b) Time evolution of $R(t)$ and $\bar{V}(t)/V_c$ averaged over 10 simulation trials with random initial conditions for three different sets of control parameters: $(n, T_f) = (3, T)$ in solid blue lines, $(n, T_f) = (8, 2T)$ in green dashed lines, $(n, T_f) = (12, 4T)$ in red dotted lines.

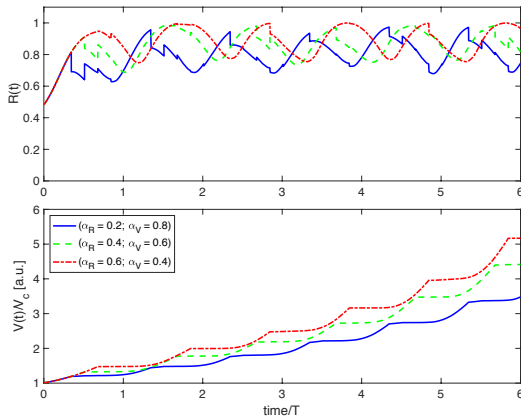
Fig. 5. Threshold control: High-variability of T_i ($CV = 22.88\%$).

only the finite prediction horizon T_p , the set \mathcal{U} is composed by 2^P possible combinations of triggers. Thus, the optimal control problem is solved by minimising the performance index J over the prediction horizon T_p . The optimisation is achieved by exploring all the possible combinations of sequence of triggers.

For the numerical analysis, we set the length of both the prediction horizon T_p and the control horizon T_c equal to the nominal cell-cycle duration T , and the number of triggers P equals to 6. To assess the feasibility of the control algorithm, a set of simulations was carried out by varying the weights α_R and α_V . Figure 6(a) shows the response of the cell population to the control input generated by the MPC algorithm with control parameters $(\alpha_R, \alpha_V) =$



(a) Time evolution of $\vartheta_i(t)$ and $\bar{V}_i(t)/V_c$, for one simulation trial, are reported in red colour. Their average values over the whole population are reported in blue. The corresponding control signal $u(t)$ generated by the MPC algorithm with weight factors $(\alpha_R, \alpha_V) = (0.4, 0.6)$ is reported in the bottom panel.



(b) Time evolution of $R(t)$ and $\bar{V}(t)/V_c$ averaged over 10 simulation trials with random initial conditions for three different sets of weight factors: $(\alpha_R, \alpha_V) = (0.2, 0.8)$ in solid blue lines, $(\alpha_R, \alpha_V) = (0.4, 0.6)$ in green dashed lines, $(\alpha_R, \alpha_V) = (0.6, 0.4)$ in red dotted lines.

Fig. 6. MPC: High-variability of T_i ($CV = 22.88\%$).

(0.4, 0.6). Examples of three time evolution of the mean phase coherence $R(t)$ and the normalised average population volume $\bar{V}(t)/V_c$ both averaged over 10 trials with random initial conditions are shown in Figure 6(b).

D. Comparative analysis

We performed a comparative analysis the three control algorithms across several simulated scenarios. For each scenario, we computed the indices J_R , J_V , and the total number of triggers applied during the simulation. Results obtained averaging over 10 trials with random initial conditions are presented in Table I.

a) *Stop&Go control*: Although this control algorithm is very simple and can guarantee a high level of synchronisation (J_R equal to 0.1821 and 0.1031 for high and low cell-to-cell

variability, respectively) reaching a regime after about one nominal period T of the cell cycle, it has the drawback of causing excessive volume growth (J_V equal to 0.0075 and 0.0009 for high and low cell-to-cell variability, respectively). Indeed, faster cells, i.e. those having a smaller cycle period T_i , reach phase 2π before the other slower cells and therefore they are stuck there growing until the next control trigger is applied, thus yielding an unnecessary volume increase.

b) *Threshold control*: This control algorithm guarantees a good level of synchronisation and it contains excessive volume growth with respect to the Stop&Go control. However, a trade-off between J_R and J_V exists in the tuning of the control parameters (n, T_f) . Specifically, low values of T_f give lower values of J_R but higher values of J_V , and vice-versa for high values of T_f . On the other hand, increasing n gives lower values of J_V but it does not result in significant reduction of J_R .

c) *MPC*: This control algorithm reaches a high level of synchronisation, limiting at the same time the volume growth. Among the control algorithms, the MPC achieves the best trade-off between the indices J_R and J_V . One drawback of the algorithm could be the computational effort needed to solve the optimal control problem in real-time. However, the assumption on the finite sequence of triggers reduces the computational time, allowing the solution of the optimal control problem to be found in few seconds.

V. CONCLUSIONS

We have presented a theoretical and experimental framework to address the cell-cycle synchronisation problem in budding yeast in the context of a real biological scenario. We characterised experimentally a yeast strain whose cell-cycle can be controlled experimentally by changing growth medium. We then derived a phase-oscillator model to describe the cell-cycle phase, as well as the volume growth dynamics. We demonstrated in-silico the feasibility of synchronizing the cell cycle across a cell population, while containing at the same time the volume growth. To this end, we devised and implemented three control algorithms: *Stop&Go control*, *Threshold control* and *MPC*. A numerical analysis was performed to assess and compare the three strategies.

Taken together all the numerical results provide evidence for the success of the proposed control approaches in living yeast cells. Nevertheless, several issues remain open both in terms of control performance and experimental implementation. Indeed, model uncertainty and parametric variability could affect the control performance, thus adaptive and robust control strategies are required. To this aim, we aim to improve the control strategies by choosing adaptively the control algorithms' parameters, e.g. α_R and α_V of MPC algorithm, or resorting to alternative heuristic strategies such as reinforcement learning control.

Finally, ongoing work is aimed at implementing and validating in-vivo the proposed control strategies which will be presented elsewhere.

TABLE I
NUMERICAL COMPARISON OF THE CONTROL ALGORITHMS.

	Control parameters	Low variability			High variability		
		J_R	J_V	# of triggers	J_R	J_V	# of triggers
Stop&Go	–	0.1031	0.0009	6	0.1821	0.0075	5
	$(n, T_f) = (3, 1)$	0.2045	0.0007	8.8	0.2865	0.0042	7.0
Threshold	$(n, T_f) = (8, 2)$	0.3667	0.0004	13.1	0.4173	0.0026	11.2
	$(n, T_f) = (12, 4)$	0.6550	0.0003	22.1	0.6854	0.0010	20.2
MPC	$(\alpha_R, \alpha_V) = (0.2, 0.8)$	0.1752	0.0009	18.8	0.3623	0.0014	19.0
	$(\alpha_R, \alpha_V) = (0.4, 0.6)$	0.1386	0.0012	16.3	0.2664	0.0026	13.3
	$(\alpha_R, \alpha_V) = (0.6, 0.4)$	0.0996	0.0016	11.3	0.2211	0.0039	7.1

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REFERENCES

- [1] P. A. Iglesias and B. P. Ingalls, *Control theory and systems biology*. MIT Press, 2010.
- [2] L. Postiglione, S. Napolitano, E. Pedone, D. L. Rocca, F. Aulicino, M. Santorelli, B. Tumaini, L. Marucci, and D. di Bernardo, “Regulation of gene expression and signaling pathway activity in mammalian cells by automated microfluidics feedback control,” *ACS Synthetic Biology*, vol. 0, no. 0, p. null, 0.
- [3] P. Harrigan, H. D. Madhani, and H. El-Samad, “Real-time genetic compensation defines the dynamic demands of feedback control,” *Cell*, vol. 175, no. 3, pp. 877–886.e10, 2018.
- [4] M. Rullan, D. Benzinger, G. W. Schmidt, A. Miliias-Argeitis, and M. Khammash, “An optogenetic platform for real-time, single-cell interrogation of stochastic transcriptional regulation,” *Molecular Cell*, vol. 70, no. 4, pp. 745–756.e6, 2018.
- [5] J.-B. Lugagne, S. Sosa Carrillo, M. Kirch, A. Köhler, G. Batt, and P. Hersen, “Balancing a genetic toggle switch by real-time feedback control and periodic forcing,” *Nature Communications*, vol. 8, no. 1, pp. 1671–1671, 2017.
- [6] R. Chait, J. Ruess, T. Bergmiller, G. Tkačik, and C. C. Guet, “Shaping bacterial population behavior through computer-interfaced control of individual cells,” *Nature Communications*, vol. 8, no. 1, pp. 1535–1535, 2017.
- [7] A. Miliias-Argeitis, M. Rullan, S. K. Aoki, P. Buchmann, and M. Khammash, “Automated optogenetic feedback control for precise and robust regulation of gene expression and cell growth,” *Nature Communications*, vol. 7, pp. 12 546–12 546, 2016.
- [8] G. Fiore, G. Perrino, M. di Bernardo, and D. di Bernardo, “In vivo real-time control of gene expression: A comparative analysis of feedback control strategies in yeast,” *ACS Synthetic Biology*, vol. 5, no. 2, pp. 154–162, 2016.
- [9] G. Charvin, F. R. Cross, and E. D. Siggia, “Forced periodic expression of g1 cyclins phase-locks the budding yeast cell cycle,” *Proceedings of the National Academy of Sciences*, vol. 106, no. 16, pp. 6632–6637, 2009.
- [10] S. J. Rahi, K. Pecani, A. Ondracka, C. Oikonomou, and F. R. Cross, “The CDK-APC/c oscillator predominantly entrains periodic cell-cycle transcription,” *Cell*, vol. 165, no. 2, pp. 475–487, 2016.
- [11] F. Menolascina, G. Fiore, E. Orabona, L. De Stefano, M. Ferry, J. Hasty, M. di Bernardo, and D. di Bernardo, “In-vivo real-time control of protein expression from endogenous and synthetic gene networks,” *PLoS Computational Biology*, vol. 10, no. 5, pp. e1 003 625–e1 003 625, 2014.
- [12] A. T. Winfree, *The Geometry of Biological Time*, 2nd ed., ser. Interdisciplinary Applied Mathematics. Springer-Verlag, 2001.
- [13] Y. Kuramoto, *Chemical Oscillations, Waves, and Turbulence*, ser. Springer Series in Synergetics. Springer-Verlag, 1984.
- [14] J. Uhlendorf, A. Miermont, T. Delaveau, G. Charvin, F. Fages, S. Bottani, G. Batt, and P. Hersen, “Long-term model predictive control of gene expression at the population and single-cell levels,” *Proceedings of the National Academy of Sciences of the United States of America*, vol. 109, no. 35, pp. 14 271–14 276, 2012.
- [15] D. Q. Mayne, J. B. Rawlings, C. V. Rao, and P. O. M. Scokaert, “Constrained model predictive control: Stability and optimality,” *Automatica*, vol. 36, no. 6, pp. 789–814, 2000.
- [16] A. Bemporad and D. Muñoz de la Peña, “Multiobjective model predictive control,” *Automatica*, vol. 45, no. 12, pp. 2823–2830, 2009.