

1 **Pilot scale study on UV-C inactivation of bacterial endospores and virus**
2 **particles in whole milk: evaluation of system efficiency and product quality**

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33 **Abstract**

34 UV-C processing of whole milk (WM) using a designed pilot scale Dean flow system was
35 conducted at flow rates (11.88, 23.77, and 47.55 gph), Reynolds number ranges from 2890-11562
36 and the Dean number (at curved region) calculated as (648-2595) to inactivate bacterial endospores
37 and virus particles. Biodosimetry studies were conducted to quantify the reduction equivalent
38 fluence at selected experimental conditions. Results revealed that the fluence distribution
39 improved as flow rate increases, attributed to increase in Dean effects and turbulence intensity.
40 Microbial inactivation studies conducted at 47.55 gph showed 0.91 ± 0.15 and 2.14 ± 0.19 log
41 reduction/ pass for *B. cereus* endospores and T1UV phage. Linear inactivation trend was observed
42 against number of passes which clearly demonstrates equivalent fluence delivery during each pass.
43 Lipid peroxidation value and volatiles profile did not change significantly at UV fluence of 60
44 mJ/cm². Lower E_{EO} value signifies the higher electrical efficiency of the system.

45 **Keywords:** Pilot scale UV system; whole milk; bacterial endospores; virus particles; lipid
46 peroxidation; volatiles profile

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56 **1. Introduction**

57 Milk and its products are the potential source of various nutrients such as lipids, proteins,
58 carbohydrates, vitamins, minerals, and enzymes; these components present in milk allows the
59 growth of numerous pathogenic microorganisms (Oliver et al., 2005; Shanmugam et al., 2012;
60 Bogahawaththa et al., 2018; Munir et al., 2019). According to Delorme et al. (2020), dairy
61 processing needs strict quality control as contamination issues can originate at any stage of the
62 food chain. The presence of aerobic spore-forming bacteria of the *Bacillus* genus in milk is
63 consider as the major cause of deterioration of raw and pasteurized milk (Crielly et al., 1994;
64 Cosentino et al., 1997). *B. cereus* is a major concern for the dairy industry because of its
65 psychrotolerant nature, which limits the shelf life of the pasteurized milk and milk products stored
66 at 6-7°C and its ability to produce toxins which makes it a potential cause for foodborne illnesses
67 where the production of emetic and enterotoxin results in vomiting and diarrhea, respectively
68 (Griffiths, 1992; Bilbao-Sáinz et al., 2009). According to CDC, more than 63000 cases of *B.*
69 *cereus* illness are reported annually in the United States and all of them are foodborne (Scallan et
70 al., 2011).

71 Pasteurization and sterilization are the most common techniques used by industries to ensure
72 the safety of milk (Bermúdez-Aguirre et al., 2009; Choudhary and Bandla, 2012; Patras et al.,
73 2020). The Code of Federal Regulations (3), Title 21, Section 131.3b, defines pasteurized dairy
74 products as using properly operated equipment to heat every particle of the product to a specified
75 temperature and held at or above that temperature for a specified time. Though these techniques
76 are efficient and can inactivate numerous foodborne pathogens ranging from vegetative cells to
77 viruses and spoilage causing enzymes. One problem that is found to cause a reduction in the shelf
78 life of WM is the presence and growth of *Bacillus* sp. and its heat resistant spores in pasteurized,

79 sterilized as well as ultra-pasteurized milk (Pettersson et al., 1996; Scheldeman et al., 2004; Cullor,
80 2011). The high pasteurization temperatures can easily destroy vegetative cells but can activate
81 the spores, which leads to germination and growth (McGUIGGAN et al., 1994). Other
82 disadvantages of pasteurization techniques are significant alteration in the sensorial and nutritional
83 profile of the product, protein denaturation, undesired changes to milk fat globules, high
84 operational and processing cost which makes it unfeasible for small scale dairy units (Garcia-
85 Amezquita et al., 2009; Cappozzo et al., 2015; Gunter-Ward et al., 2018). Raw dairy products are
86 prioritized by the consumers because of their typical sensorial characteristics and other health
87 benefits such as decreased incidence of asthma, allergies, and respiratory infections which suggest
88 immune benefits of dairy proteins are lost upon heat processing (Buchin et al., 1998; Braun-
89 Fahrländer and Von Mutius, 2011). To preserve the benefits of raw dairy products without
90 compromising the safety warrants the study of non-thermal technology for processing of dairy
91 products (Gunter-ward et al., 2018). Interest in light-based technologies (UV-C irradiation) for
92 liquid food processing has exponentially grown over the years is increasing due to lower energy
93 consumption, cost-effectiveness, minimal effect on the quality of the products (Tran and Farid,
94 2004; Keyser et al., 2008; Corrales et al., 2012; Feng et al., 2013; Ochoa-Velasco et al., 2014;
95 Jermann et al., 2015; Islam et al., 2016). Several federal agencies have approved the use of UV-C
96 technology for milk treatment. For example, European Food Safety Authority (EFSA) approved
97 the use of UV-C at 253.7 nm for milk processing post pasteurization for the extension of shelf life
98 and to improve the nutritional value as it increases the vitamin D3 content in the product (EFSA,
99 2016, and Koutchma, 2018). Food Safety and Standards Authority of India approved the UV-C
100 processing of raw milk processed via the Sure Pure UV system (Koutchma, 2018). In USA, any
101 new technology for processing of grade A milk has to go through PMO and FDA clearance.

102 Many lab-scale studies on the UV-C processing of milk revealed the efficiency of the process
103 (Choudhary et al., 2011; Bandla et al., 2012; Gunter-ward et al., 2018; Ansari et al., 2019). Still,
104 the major challenges at the pilot scale are limited light penetration and mass transfer (Sizer and
105 Balasubramanian, 1999) and fluence delivery per single pass. Milk is an opaque fluid with high
106 absorption as well as scattering coefficient due to the presence of lipids, proteins and vitamins.
107 UV light is absorbed by these micro and macro nutrients and creates UV gradients (Walstra and
108 Jenness, 1984). Some studies reported that the major problem of UV-C processing is oxidation of
109 fats and off-flavors (Bekbölet, 1990; Matak et al., 2005, 2007). However, the use of an efficient
110 reactor design can improve mass transfer and mix the bulk field homogenously overcoming those
111 challenges, delivering a uniform UV fluence (Koutchma, 2009). It is quite evident in the literature
112 that Dean flow reactor is an efficient design where additional turbulence is generated when fluid
113 passes through the coiled tube (Dean, 1927; Gopisetty et al., 2018; Vashisht et al., 2021). This is
114 known as the Dean effect, and it is produced by the curvature radius between the inner and outer
115 boundary layer (Dean, 1927). In our previous study we used a simulated fluid and scientifically
116 proved that the Dean flow UV reactor distributes the fluence homogeneously demonstrated by the
117 linear microbial inactivation kinetics (Vashisht et al., 2021). In reactor engineering, it is crucial to
118 ensure that all the fluid particles receive the UV fluence within the acceptable limit i.e. minimal
119 product damage and efficient microbial inactivation. An understanding of the fluid mechanical and
120 flow properties is extremely important. Herein, we will evaluate the peroxidation and volatiles of
121 WM, confirming the UV fluence (pasteurization equivalent dose). We hypothesize that effective
122 fluence delivery in the system can inactivate the pathogens and preserve the quality of the product.
123 The objectives of the present study are i) validation of the pilot-scale Dean flow UV system using

124 biosimetry approach, ii) evaluation of the microbial inactivation kinetics, iii) assessment of the
125 volatile profile and lipid peroxidation of the UV irradiated whole milk.

126 **2. Materials and Methods**

127 2.1. Bacteriophage and endospores propagation

128 T1UV bacteriophage and *Bacillus cereus* ATCC 14579 endospores were used in this study. T1
129 UV culture (@ 10^{10} pfu/mL) was purchased from GAP EnviroMicrobial Services Limited, London,
130 ON, Canada and *Bacillus cereus* ATCC 14579 was obtained from American Type Culture
131 Collection (ATCC) center (Manassas, VA). Culturing of endospores was conducting using a Bacto
132 Brain Heart Infusion Broth (BHI, Beckton, Dickinson, Franklin Lakes, NJ) as a growth medium,
133 incubation was done at 37 °C with aeration at 180 rpm. Nutrient-rich, a chemically defined medium
134 known as Mineral Salts Medium (MSM) was used for sporulation. 20 mL of overnight grown
135 culture was inoculated in 200 mL of MSM in 1 L of the flask. Incubation was be done at 30 °C
136 with aeration at 180 rpm for 3 days. Dormant spores were purified by suspending the pellets in
137 20% Nycodenz (VWR, Atlanta, GA) followed by 50% Nycodenz density gradient centrifugation
138 at 14000 g for 45 minutes. Enumeration was done using a standard plate count method.

139 2.2. Optical properties

140 Optical properties (absorbance and reduced scattering) of the WM were evaluated at 254 nm
141 by using a double beam spectrophotometer connected to a 6-inch integrating sphere. Inverse
142 adding doubling technique was used to quantify the absorption coefficient, scattering coefficient,
143 base-e. A series of thin quartz cuvettes were used to achieve a light transmission between 10 to
144 14%. A MS-DOS based code was run to separate the absorption coefficient and reduced scattering
145 coefficients. Light absorption and reflection were accounted for in the calculations.

$$146 \text{ Transmittance } \left(\frac{\%}{\text{cm}} \right) = (10^{-A}) \times 100 \quad (1)$$

147 where A stands for the absorbance (base 10) of the sample at 254 nm for a 1 cm path length. pH of
148 the product was measured by using a pH meter (Jenway, Cole Palmer, OSA, UK). All the
149 measurements were taken in triplicate to reduce error.

150 2.3. Organism sensitivity test

151 *Bacillus cereus* ATCC 14,579 and T1UV phage were evaluated for D_{10} values (dose required
152 for 90 % inactivation or 10 % survival). Microorganisms were inoculated separately ($@10^6$ - 10^7
153 CFU/mL or PFU/mL) in whole milk. The absorption coefficient of the final solution was measured
154 using the UV-Vis. spectrophotometer (Thermo Scientific, Genesys 10S, Milwaukee, WI, US).
155 Known UV fluence were delivered (3, 6, and 9 mJ/cm²) for both the microorganisms (Bolton and
156 Linden, 2003). 5 mL of sample was exposed to UV using a Collimated Beam Apparatus (Trojan
157 Technologies, London, ON, Canada), which contains a 25 W low-pressure mercury lamp. The
158 suspension was stirred during irradiation using a magnetic stirrer to ensure equal UV volatil to all
159 microorganisms. The D_{10} value was evaluated using the LINEST function of Microsoft Excel
160 between the UV fluence delivered, and the log inactivation obtained. All the experiments were
161 done in triplicate to reduce the error

162 2.4. UV- C Treatment

163 WM was exposed to UV-C light using the Dean flow UV system (Fig. 1). The system is a
164 continuous UV reactor, consisting of a 500W low-pressure mercury lamp protected with stainless
165 steel cylindrical blocker, a cooling fan, and a food-grade FEP (Fluorinated Ethylene Propylene)
166 tube. The tube length is 26 m with an inner diameter (D_i) of 0.64 cm, an outer diameter (D_o) of
167 0.74 cm, a wall thickness of 0.5 mm. The tube was wrapped around the centrally positioned lamp
168 in a serpentine path. The diameter of the coil (D_c) was 12.7 cm. The tubing was carefully
169 engineered to have significant curves (bends) to induce mixing. The system also included a 4–20

170 mA current loop receiver and an indicator for output power lamp display. The electric supply of
171 220 V (single phase), 60 Hz was used. The irradiance at the surface of the FEP tube was 22
172 mW/cm², measured using an International Light Technologies (Peabody, MA) IL-1700 radiometer
173 with a SED 240 detector fitted with a NS254 filter. Transmittance (UVT%) of FEP tube was 65%,
174 measured using a UV–Visible Spectrophotometer (Thermo Scientific, Genesys 10S, Milwaukee,
175 WI, US). Therefore, the calculated UV intensity at the surface of the fluid was 14.3 mW/cm². The
176 total reactor volume was 0.80 L. The system was connected to an inlet, outlet, and a rinse tank (20
177 L each). The output power at 254 nm was approximately 220 Watts at 254 nm. WM was treated
178 at a flow rate of 0.75, 1.5, and 3 L/min (equivalent to 11.88, 23.77, 47.55 gph, respectively). The
179 flowrate was controlled by Watson Marlow 730U peristaltic pump (Watson Marlow, Charlotte,
180 NC, US). The pump was validated by using a bucket test in which time to collect a known volume
181 of the fluid was estimated. CIP was done before starting the experiment as well as at the end. All
182 experiments were conducted in triplicated to reduce random error. Dean number (De) evaluated as
183 a function of Reynolds number (Re) and the geometric parameters D and D_c, which stands for the
184 hydraulic diameter of the tube (m) and diameter of the coil (m), respectively (Gopisetty et al.,
185 2018, 2019). The following equation was used:

$$186 \quad D_e = R_e \left(\frac{\sqrt{D}}{D_c} \right) \quad (2)$$

187 Where Reynolds numbers (R_e) was evaluated as:

$$188 \quad R_e = \frac{\rho V D}{\mu} \quad (3)$$

189 where ρ denotes the fluid density, μ denotes the dynamic viscosity, V is the fluid velocity, and D
190 denotes the diameter of the tube. The R_e of < 2100 represents laminar flow pattern, R_e between
191 2100-4000 shows transient flow conditions, and R_e of > 4000 means turbulent flow conditions
192 (Bandla et al., 2012; Pendyala et al., 2021; Vashisht et al., 2021). The residence time (RT) was 64,

193 32 and 16 seconds for 0.75 L/min. (11.88 gph), 1.5 L/min. (23.77 gph) and 3 L/min. (47.55 gph)
194 respectively, which was evaluated by using the following equation:

$$195 \quad RT = \frac{V}{Q} \quad (4)$$

196 Where V is the volume (L); Q is the flow rate (L/min) Average flow velocity (vf) (m/sec.) was
197 evaluated by using the following equation:

$$198 \quad V_f = \frac{Q}{\pi r^3 \times 60 \times 10^3} \quad (5)$$

199 Q is the flow rate of fluid in L/min. r is the tube's radius in m.

200 2.5. Determination of volatiles using electronic nose

201 Volatiles were evaluated by using an electronic nose (Heracles II, Alpha MOS, Toulouse,
202 France). It consists of two columns working in parallel mode: a non-polar column (MXT5: 5%
203 diphenyl, 95% methylpolysiloxane, 10 m length and 180 μm diameter). The volatiles profile of
204 treated samples (at 60 and 120 mJ/cm^2 of fluence) was compared with controlled (untreated)
205 samples. 20 mL of vials were filled with 10 mL of the sample followed by sealing with septa screw
206 cap using a crimper. The vials were equilibrated for 200 seconds at 50 $^\circ\text{C}$ in agitation chamber.
207 Autosampler was used to inject the generated headspace aroma into the electronic nose column at
208 a flow rate of 270 $\mu\text{L}/\text{s}$. The column temperature program was 40 $^\circ\text{C}$ (1 min) – 2 $^\circ\text{C min}^{-1}$ – 200 $^\circ\text{C}$
209 (3 min). The temperature of injector and detector was set at 180 $^\circ\text{C}$ and 220 $^\circ\text{C}$, respectively. The
210 chromatograms were obtained using Flame ionization detector (FID) and individual volatile profile
211 including Kovats index, retention time and sensory description was evaluated by using
212 AromaChemBase software. The analysis was done by using Alpha Soft (Alpha Soft version 3.0.0,
213 Toulouse, France). All the samples were evaluated in triplicate to reduce error and all the values
214 were mentioned in terms of relative area.

215 2.6. Determination of lipid peroxidation

216 Lipid peroxidation value was evaluated by a standard curve method using spectrophotometer.
217 According, to Matak et al. (2007) value is measured in terms of MDA (malondialdehyde) and other
218 reactive substance so standards of 50, 25, 12.5, 6.25, 3.125 μM concentrations were prepared using
219 MDA. 1 mL of irradiated whole milk was mixed and vortexed with 7 mL of 1% phosphoric acid
220 followed by the addition of 2 mL of 42 mmol/L TBA (thiobarbituric acid). The solution was heated
221 at 100°C for 60 minutes followed by cooling it down (by keeping on ice). The color was changed
222 to pink, where the intensity was dependent upon the extent of lipid peroxidation. 4 mL of solution
223 was added to the 4 mL of 1:12 mixture of 2 mol/L sodium hydroxide and methanol, it was vortex
224 mixed for 10 seconds followed by centrifugation at 13000 g for 3 minutes. Supernatant was
225 evaluated for absorbance at 532 nm using a UV-Vis spectrophotometer (Thermo Scientific,
226 Genesys 10S, Milwaukee, WI, US) calibrated against blank.

227 2.7. Electrical energy per order (E_{EO})

228 E_{EO} was estimated to measure the kilowatt-hours of energy required to reduce the microbial
229 population by one log (Bolton, 2010). This term is commonly used to assess electrical energy
230 efficiency (Ward et al., 2019). E_{EO} value depends upon the nature of fluid under processing and
231 the geometry of the reactor (Pendyala et al., 2021). Evaluation was done by using the equation
232 given by Ward et al. (2019).

$$233 E_{EO} = \frac{P_{UV}}{F \times \log \frac{C_0}{C_t}} \quad (6)$$

234 where P_{UV} refers to the power of the electric lamp or total energy of the lamp and power supply
235 (kW), F stands for volumetric flow rate (m^3/h .), and C_0 and C_t stand for initial and final microbial
236 concentration, respectively.

237 2.8. Statistical Analysis

238 All the treatments were conducted in replicates where each sample was independent and
239 randomly assigned. All the values are reported as mean \pm std. deviation. For evaluation of effect
240 of numerous treatments on REF, inactivation kinetics, lipid peroxidation and volatiles profile one-
241 way ANOVA along with the Tukey HSD (honestly significant difference) at $p < 0.05$ significance
242 level.

243 **3. Result and Discussion**

244 3.1. Optical properties of test fluid

245 Optical properties of WM are illustrated in Table 1. The absorption and reduced scattering
246 coefficient were measured as $23.7 \pm 0.3 \text{ cm}^{-1}$ (transmittance - $2.5\text{E-}22 \text{ %/cm}$) and $42.3 \pm 0.5 \text{ cm}^{-1}$
247 respectively, with 12 % reflectance. The pH and fat content of the WM was 6.73 ± 0.17 and 3.27
248 %, respectively. Previous studies evaluated the absorption coefficient of whole milk without
249 separating the reduced scattering coefficient and reported significantly higher values, 220 cm^{-1}
250 (Choudhary et al., 2011), $326 \pm 1.5 \text{ cm}^{-1}$ (Ansari et al., 2019). Optical properties clearly show the
251 opaque nature of the test fluid. WM significantly absorbs and scatters the UV photons. Suspended
252 particles are mainly responsible for attenuation of UV light via scattering effect (Gunter-ward et
253 al., 2018). If the product particles are larger than the UV wavelength then it leads to the forward
254 scattering with amplified back scattering effect (Koutchma, 2009). Our results demonstrate high
255 scattering effect of WM, due to fat globules and proteins (micellar casein) as reported in the
256 literature (Gunter-ward et al., 2018; Ward et al., 2019). There could be a minor scattering effect
257 due to dissolved minerals and sugar (lactose), however it can be ignored because their
258 proportionate size is lesser than the fat and protein components (Gastélum-Barrios et al., 2020).

259 3.2. Design and Development of dean flow reactor

260 Many literature studies used circular path coiled tube dean flow UV systems to evaluate
261 microbial inactivation in milk (Choudhary et al., 2011; Bandla et al., 2012; Ansari et al., 2019).

262 To improve the Dean forces, in our previous proof-of-concept study we designed and developed
263 pilot scale serpentine path coiled Dean flow UV system and evaluated its microbial inactivation
264 efficiency. Previously, we irradiated fluids with absorption coefficient ranging from 6.5 to 17 cm⁻¹
265 ¹ at commercial flow rates (Vashisht et al., 2021) and evaluated the system performance. In the
266 current study, the system was challenged against a highly opaque fluid such a WM with an
267 absorption coefficient of 23.7 cm⁻¹. The initial design of the system consisted of a Teflon tubing
268 (45% UV transmission) of 1 cm path length, 20 m total length and 18 cm coil diameter (Vashisht
269 et al., 2021). The reactor system was modified where FEP tubing (65% UV transmission) was used
270 to have high transmittivity. Tube length was increased to 26 m to increase the residence time and
271 UV fluence/pass. The optical thickness of the fluid was reduced to 0.64 cm. This will allow higher
272 penetration of photons in the bulk fluid. The coil diameter was reduced to 12.7 cm to increase the
273 Dean effect (as Dean number is inversely proportional to coil diameter). The ratio of D to D_c
274 (where D stands for inner diameter of tubing (0.64 cm), and D_c stands for the diameter of coil
275 (12.7 cm)) of the designed reactor was 0.050 (0.64/12.7), which was in the range of 0.03–0.10
276 demonstrating the initiation of Dean flow vortices during the experiments (Koutchma, 2009).
277 Bandla et al. (2012) used Reynolds number as a parameter of turbulence but missed to evaluate
278 the Dean number. This number is a significant parameter as it generates the additional turbulence
279 hence the efficient mixing conditions (Dean 1927, Gopisetty et al., 2018, 2019). The evaluated
280 Reynolds and Dean number for each flow rate was in the range of 2890-11562 and 648-2595,
281 respectively (Table 2). This data revealed that the experiments were conducted at transient to fully
282 turbulent conditions to provide efficient mass transfer (Dean, 1927; Patras et al., 2020). Turbulent
283 flow conditions deliver higher velocity to the particles as compared to the mean velocity of
284 individual particles providing efficient UV fluence distribution (Koutchma, 2009). Volume

285 average UV intensity depends on the relative positions of the particle and the UV lamps
286 orientation. The UV fluence received by the micro-organisms depends on two main factors: the
287 trajectories through the system and the REF rate (Vashisht et al., 2021). The incident radiation rate
288 is dependent on the positions of the UV lamps within the UV system.

289 3.3. UV fluence validation at experimental flow rates

290 Biodosimetry study was conducted using *B. cereus* endospores to quantify delivered UV
291 fluence. The D_{10} value of *B. cereus* endospore was quantified using a standard collimated beam
292 system as 8.91 ± 0.07 mJ/cm², it was within the range as reported in the literature (Gopisetty et al.,
293 2018; Pendyala et al., 2019, 2020, 2021). WM was inoculated with *B. cereus* (10^7 cfu/mL) and it
294 was passed through the UV systemlight at flow-rates of 0.75 L/min. (11.88 gph), 1.5 L/min. (23.77
295 gph) and 3 L/min. (47.55 gph). REF was evaluated as a product of D_{10} value and log reduction
296 ($\text{Log}N_0-N$). Total REF was 26 ± 1.07 , 14.5 ± 0.53 and 10 ± 0.27 mJ/cm² at 11.88, 23.77 and 47.55
297 gph of flow rate, respectively. It was observed that with the increase in flow rate, total REF was
298 significantly reduced due to lower hydraulic retention times (Fig. 2a). In contrast, the REF rate
299 (REF per sec.) was observed to be increase with the increase in flow rate attributed to the increase
300 in turbulence and Dean forces intensity as demonstrated by the increased Reynolds and Dean
301 number (Fig. 2b). Similar trends were reported by previous authors (Gunter-Ward et al., 2018;
302 Ansari et al., 2019; Vashisht et al., 2021). According to Vashisht et al. (2021) Dean number plays
303 a pivotal role in UV fluence distribution while the residence time directs the total REF for the
304 inactivation of microbes hence a balance needs to be maintained between these process parameters.
305 Herein, REF rate can be a useful factor for the determination of system's performance in terms of
306 fluence distribution which is critical at commercial level. At 47.55 gph flow rate, the REF rate was
307 1.54 and 1.38 times efficient than the 11.88 and 23.77 gph of flow rate. UV-C systems are suitable

308 for the treatment of opaque liquids when efficient mixing conditions that can surpass the potent
309 intensity gradient and ensure effective fluence distribution (Vashisht et al., 2021). Inefficient
310 mixing conditions will significantly affect the UV system performance and will result in non-linear
311 inactivation kinetics of the target pathogen (Atilgan, 2013; Crook et al., 2015). Completing
312 understanding of the UV system performance, knowledge of optical properties of the test fluids
313 will allow accurate sizing of UV systems.

314 3.4. Microbial Inactivation studies

315 Since better system performance was observed at higher flow rate, microbial inactivation
316 studies were conducted at a flowrate of 47.55 gph using *B. cereus* endospores and T1UV virus
317 particles (selected as a surrogate to *Salmonella*, *Listeria* and *Cronobacter*). Selection of pertinent
318 microorganism is of utmost importance during validation studies (Patras et al., 2020). *B. cereus*
319 endospores are most common pertinent bacterial spores present in milk and causes food safety and
320 spoilage issues (Choudhary et al., 2011, Gunter-Ward et al., 2018; Patras et al., 2020) while
321 *Salmonella* & *Listeria* are the pertinent vegetative microorganisms in milk (Patras et al., 2020).
322 The D_{10} value of T1UV phage is similar to *Salmonella* and *Listeria* and therefore used in this
323 research study. 0.91 ± 0.15 and 2.14 ± 0.19 log reduction per pass ($R^2 > 0.99$, $p < 0.05$) was
324 observed for *B. cereus* and T1UV phage, respectively (Fig. 3a and 3b). Linear trend demonstrates
325 uniform REF delivery during each pass. The kinetics of the UV inactivation are widely assumed
326 for a first-order reactions with respect to the REF. The typical UV response curve can be
327 represented in two ways: a log survival curve and a log inactivation curve

328 It is quite evident if the system is not efficient and does not provide good mixing conditions,
329 then the desired UV fluence will not be delivered to the microbes which may result in lower
330 inactivation rate at higher UV fluence (Bhullar et al., 2019) and tail may be observed in inactivation

331 curve. For instance, Makarapong et al. (2020) reported 4.7 and 4.6 log reduction of total microbial
332 count in WM treated with 98 and 110 mJ/cm² of UV fluence. In our studies total log reduction of
333 *B. cereus* and T1 UV phage were 2.75± 0.01 and 4.29 ± 0.09 after three and two passes,
334 respectively. Previous Dean concept studies reported a significant log reduction of pathogenic
335 microbes in dairy products. Ansari et al. (2019) reported *B. cereus* endospores log reduction of 6,
336 2.90 and 1.1 in skim, cow and bovine milk, respectively where UV-C processing was used as
337 hurdle technology. Bandla et al. (2012), reported 2.3 log reduction of standard plate count in raw
338 cow milk given a UV-C fluence of 16.82 mJ/cm². Matak et al. (2005) reported 5-log reduction of
339 *Listeria monocytogenes* in goat milk given a UV-C fluence of 15.8 ± 1.6 mJ/cm² but the
340 inactivation kinetics reported was non-linear which demonstrates that author failed to achieve
341 efficient mixing conditions. Crook et al. (2015) used thin film reactor and reported 5-log reduction
342 of *Listeria monocytogenes* and *Staphylococcus aureus* in WM, but the fluence was reported in J/L
343 which is disparate to the commonly used standard unit i.e., mJ/cm². In our previous studies we
344 introduced the concept of Pasteurization and Sterilization Equivalent Dose referred to the fluence
345 required for 5 log reduction of *S. Typhimurium* and 6 log reduction of *B. cereus* endospores,
346 respectively (Vashisht et al., 2021). Therefore, in our studies at 47.55 gph of flow rate, 3 and 7
347 passes are sufficient to provide a pasteurization and sterilization equivalent dose, respectively
348 while another approach could be scaling up and increasing the length of tubing of the present
349 system to increase the residence time and hence the delivered fluence per pass.

350 3.5. Lipid peroxidation

351 Milk consists of photosensitizers compounds such as riboflavin which can cause lipid
352 peroxidation during UV-C light exposures and can deteriorate the quality and limits the shelf life
353 of the dairy products (Bekbolet, 1990). The product of these reactions are hydroperoxides that can

354 decompose and form free-radicals which further causes auto oxidation and formation of off-
355 flavoring compounds (Bekbolet, 1990). The oxidation reactions are prompt and usually take place
356 when milk is exposed to metal surface or light (van Aardt et al., 2005). According to Cadwallader
357 and Howard, 1998 autoxidation and light induces oxidation of unsaturated fatty acids of milk are
358 primarily responsible for the origination of off flavor and reduction in nutritive compounds like
359 ascorbic acid and riboflavin. Literature studies reported that the extent of lipid peroxidation is
360 directly proportional to riboflavin content, and it is significantly affected by the exposure to UV
361 light photons (van Aardt et al., 2005). In our studies the pertinent microorganism was *B. cereus*.
362 Hence, sterilization equivalent dose for *B. cereus* was 53.46 mJ/cm² (6 x 8.91 mJ/cm²) (Vashisht
363 et al., 2021). Therefore 60 mJ/cm², 120 mJ/cm² and 180 mJ/cm² of UV fluence were selected for
364 lipid peroxidation studies. The temperature during the UV light exposures processing was
365 maintained at 4 °C to nullify the effect of lipase activity on fatty acids in WM (Deeth and Fitz-
366 Gerald, 1995). Fig. 4 demonstrates the increase of lipid peroxidation in a polynomial trend (2 order
367 equation) with the increase in the delivered UV fluence. Controlled samples had positive MDA
368 value (0.110 ± 0.002 µM), which shows that the lipid peroxidation was initially present in the WM.
369 At UV-C fluence of 60, 120 and 180 mJ/cm², MDA concentration was 0.114 ± 0.004, 0.138 ±
370 0.005, and 0.168 ± 0.002 µM, respectively. Fig 4b demonstrates that there was no significant
371 difference (p<0.05) between the MDA concentration of the controlled samples and the samples
372 treated with UV-C fluence of 60 mJ/cm², enough to inactivate 6.73-log of *B. cereus* and 12.58-log
373 of T1 phage. Makarapong et al. (2020) reported a significant lipid peroxidation in WM samples
374 treated with 98 and 110 mJ/cm² of fluence. However, the evaluated fluence was significantly
375 higher for the pasteurization equivalent dose reported in this study.

376 3.6. Volatiles Profile

377 Table 3 represents the volatiles profile of the untreated and irradiated WM samples. The
378 irradiated samples were exposed to UV fluence of 60 and 120 mJ/cm² fluence prior to the
379 evaluation of their volatiles profile. Overall, aldehyde concentration was not significantly ($p >$
380 0.05) affected UV irradiated samples. Primary aldehydes present in untreated samples were 2-
381 methylpropanal, butanal, and acetaldehyde, while in irradiated samples, pentanal, hexanal, and
382 butanal were majorly present. According to Kim and Morr (1996), hexanal can originally be
383 present in the milk while its formation and overall concentration can be increased by the lipid
384 peroxidation caused by the UV light treatment. Similar results were observed in our studies. There
385 was a significant difference ($p > 0.05$) in overall alcohol concentration in irradiated samples where
386 1-propanol, n-butanol, and 1-hexanol were major contributors. Among ketones, butane-2,3-dione
387 was majorly present in untreated samples, and its concentration relatively decreased in both
388 irradiated samples (Vazquez-Landaverde et al., 2006). Pereda et al. (2008) reported only one
389 carboxylic acid, i.e., hexanoic acid, in their study because of their less volatility and inefficiency
390 of the system to extract these compounds. In our experiment, we detected seven of them where the
391 major contributor was 2-methyl propanoic acid. Alteration in terpenes was not significant ($p >$
392 0.05) in irradiated samples treated with 60 mJ/cm² of UV fluence (Toso et al., 2002). Overall, there
393 was no significant ($p > 0.05$) difference in overall concentration of aldehydes, ketones, and
394 terpenes of untreated and irradiated samples that received 60 mJ/cm² of UV fluence; however,
395 increase in overall alcohols and esters and decrease in overall carboxylic acids concentration was
396 observed which may be the consequences of light reactions.

397 3.7. Electrical Energy per order (E_{EO}) evaluation

398 The evaluated E_{EO} values for both T1 UV phage and *B. cereus* at 47.55 gph of flow rate are
399 shown in Table 4. T1 UV phage had lower E_{EO} value as compared to *B. cereus* attributed to its

400 lower D_{10} value. Lower E_{EO} value demonstrates the higher efficiency of the system. Since each
401 microorganism has specific UV sensitivity (D_{10} value), E_{EO} value significantly varies with
402 geometric parameters, design of reactor, processing conditions and nature of fluid under testing
403 (Pendyala et al., 2021, Vashisht et al., 2021). E_{EO} value of *B. cereus* was evaluated for each flow
404 rate (Table 4), where it was observed to be decreasing with the increased flow rate attributed to
405 uniform distribution of fluence because of increased turbulence and Dean effect resulted in
406 increased inactivation kinetics. This proves the efficiency of system was more at highest flow rate
407 (47.88 gph) as compared to the lowest one (11.88 gph). At high flow rate two or more reactors are
408 recommended in a series to increase the residence time and hence to deliver the targeted UV
409 fluence. Therefore, a balance needs to be maintained between the chosen flow rate and number of
410 reactors required in a series.

411 **4. Conclusion**

412 A Dean flow UV system was evaluated and experimentally studied using WM as a test fluid
413 due to its high scattering coefficients. Biodosimetry studies were conducted and test results showed
414 that 47.55 gph of flow was the most efficient experimental flow rate for the coiled geometry. Linear
415 inactivation trends were observed for *B. cereus* and T1UV phage demonstrating equivalent fluence
416 during each pass. Lower E_{EO} value also signifies the higher electrical efficiency of the system.
417 Further studies revealed that at 60 mJ/cm^2 no significant effect on lipid peroxidation and volatiles
418 profile was observed. The reported fluence is enough to inactivate 7.18 log population of *B. cereus*
419 and 12.57 log of T1UV phage. Therefore, it can be concluded that commercial scale UV-C
420 processing of opaque fluids like WM is feasible using an efficient reactor design such as Dean
421 flow system. Further studies on sensory quality of UV exposed WM is warranted in the future.

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598 **Figure legends**

599 **Fig. 1.** Experimental setup of Dean flow UV system.

600 **Fig. 2.** Effect of flow rate on delivered fluence (bio studies) a) REF b) REF rate

601 Note: REF rate = REF/residence time

602 **Fig. 3.** Microbial inactivation per each pass of WM a) *B. cereus* endospores b) T1UV phage

603 **Fig. 4.** Variation of malondialdehyde concentration in irradiated milk samples with respect to the
604 delivered UV fluence.

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610 **Tables**

611 **Table 1.** Optical and Physio-chemical properties of whole milk

Optical Properties	Value	Units
Absorption coefficient	23.7 ± 0.3	cm ⁻¹
Scattering coefficient	42.3 ± 0.5	cm ⁻¹
Transmittance	2.5E-22	%
Physio-chemical properties		
Refractive Index (at 254 nm)	1.35	
pH	6.73 ± 0.17	
Fat	3.27	%

612 Data reported as mean±stdev

613

614 **Table 2.** Flow properties of the WM under testing

Flow rate (L/min.)	Residence time (sec.)	Velocity of flow (m/sec.)	Reynolds number	Dean number
0.75	64	0.39	2890	648
1.5	32	0.78	5781	1297
3	16	1.55	11562	2595

615

616 **Table 3.** Volatiles profile comparison of the untreated milk samples with irradiated samples treated
617 with UV fluence of 60 and 120 mJ/cm².

Volatiles	Control (untreated Raw milk)	Treatments	
		UV Fluence	
		60 mJ/cm ²	120 mJ/cm ²
Aldehydes			
2-methylpropanal	12.37 ± 1.32 ^a	4.28 ± 0.03 ^b	3.14 ± 0.0 ^c
Butanal	7.45 ± 0.06 ^a	4.90 ± 0.14 ^b	6.05 ± 0.49 ^a
Acetaldehyde	5.12 ± 0.18 ^a	3.35 ± 0.18 ^b	2.39 ± 0.13 ^c

Pentanal	2.12 ± 0.01^a	9.30 ± 0.18^b	10.15 ± 0.15^c
Hexanal	1.77 ± 0.06^a	6.93 ± 0.00^b	6.36 ± 0.36^b
Heptanal	1.57 ± 0.05^a	2.45 ± 0.15^b	2.50 ± 0.17^b
Citronellal	1.16 ± 0.35^a	-	0.40 ± 0.08^b
Octanal	0.91 ± 0.08^a	0.56 ± 0.15^b	0.46 ± 0.09^c
2-Decenal	0.74 ± 0.02^a	-	-
3-methyl butanal	0.58 ± 0.03^a	-	-
Total	34.27 ± 1.84^a	34.61 ± 0.70^a	35.09 ± 1.36^a
Alcohols			
1-Propanol	6.32 ± 0.37^a	7.90 ± 0.27^b	7.82 ± 0.37^b
n-butanol	5.83 ± 0.61^a	12.78 ± 0.08^b	13.88 ± 0.57^b
1-Hexanol	3.60 ± 0.28^a	5.36 ± 0.19^b	2.12 ± 0.33^a
3-heptanol	2.01 ± 0.04^a	1.43 ± 0.06^b	1.09 ± 0.07^c
1-nonanol	1.47 ± 0.06^a	-	-
Methyl eugenol	1.44 ± 0.60^a	1.49 ± 0.24^a	1.59 ± 0.00^b
Ethyl propanoate	0.48 ± 0.03^a	3.40 ± 0.02^b	4.11 ± 0.05^c
1-Decanol	0.44 ± 0.03^a	-	-
1-octanol	0.36 ± 0.10^a	-	-
Total	21.95 ± 1.21^a	32.36 ± 0.60^b	30.61 ± 1.54^b
Ketones			
butane-2,3-dione	2.98 ± 0.25^a	1.73 ± 0.01^b	1.67 ± 0.00^b
Pentan-2-one	1.59 ± 0.01^a	1.31 ± 0.02^b	1.4 ± 0.01^b
Delta Nonalactone	1.52 ± 0.26^a	2.19 ± 0.14^b	1.18 ± 0.15^c
Nonan-2-one	1.32 ± 0.39^a	1.17 ± 0.00^a	1.08 ± 0.08^a
Butan-2-one	1.21 ± 0.04^a	1.21 ± 0.04^a	1.60 ± 0.11^b
2,3-Pentanedione	0.82 ± 0.03^a	1.3 ± 0.02^b	1.37 ± 0.31^b
2-Heptanone	0.61 ± 0.03^a	0.55 ± 0.07^a	0.51 ± 0.03^a
Undecan-2-one	0.63 ± 0.02^a	0.63 ± 0.34^a	0.52 ± 0.17^a
Total	10.68 ± 0.95^a	10.09 ± 0.55^a	9.33 ± 0.52^b
Esters			
Methyl	5.09 ± 0.06^a	2.06 ± 0.10^b	1.64 ± 0.0^c

2-methylbutanoate			
Butyl acetate	1.68 ± 0.08 ^a	1.31 ± 0.04 ^b	1.15 ± 0.04 ^c
Ethyl isobutyrate	1.24 ± 0.18 ^a	2.00 ± 0.05 ^b	1.1 ± 0.03 ^a
Ethyl butyrate	1.18 ± 0.12 ^a	4.79 ± 0.15 ^b	6.34 ± 0.25 ^c
Isopropyl acetate	0.43 ± 0.10 ^a	3.38 ± 0.08 ^b	2.91 ± 0.40 ^c
Ethyl Acetate	0.83 ± 0.07 ^a	-	-
Isoamyl acetate	0.75 ± 0.10 ^a	0.86 ± 0.03 ^a	0.88 ± 0.37 ^a
Butyl butanoate	0.58 ± 0.21 ^a	-	-
ethyl heptanoate	0.49 ± 0.02 ^a	-	-
Total	12.27 ± 0.64 ^a	14.5 ± 0.45 ^b	14.02 ± 0.97 ^c
Carboxylic acid			
2-methylpropanoic acid	4.18 ± 0.28 ^a	5.38 ± 0.01 ^b	5.95 ± 0.20 ^b
Acetic Acid	1.67 ± 0.07 ^a	-	-
Propanoic acid	0.81 ± 0.31 ^a	-	-
Hexanoic acid	0.62 ± 0.01 ^a	0.57 ± 0.17 ^a	0.50 ± 0.17 ^b
Octanoic Acid	0.84 ± 0.13 ^a	0.59 ± 0.23 ^b	0.59 ± 0.07 ^b
Butanoic acid	0.92 ± 0.01 ^a	-	-
Dodecanoic acid	0.31 ± 0.05 ^a	-	-
Total	9.35 ± 0.71 ^a	6.54 ± 0.27 ^b	7.04 ± 0.31 ^c
Terpenes			
α-Terpinene	0.84 ± 0.02 ^a	0.94 ± 0.19 ^a	2.12 ± 0.01 ^b
α- Phellandrene	1.38 ± 0.23 ^a	1.45 ± 0.61 ^a	1.67 ± 0.15 ^a
Total	2.22 ± 0.25 ^a	2.39 ± 0.80 ^a	3.79 ± 0.14 ^b
Grand Total	90.26 ± 1.31 ^a	97.09 ± 0.77 ^b	95.76 ± 2.38 ^c

618 Values are mean ± standard deviation, n = 3, mean values in a row with different letters are
 619 significantly different at p < 0.05.

620

621 **Table 4.** E_{EO} of a Dean flow system to inactivate targeted microorganism under flow rate

622 conditions.

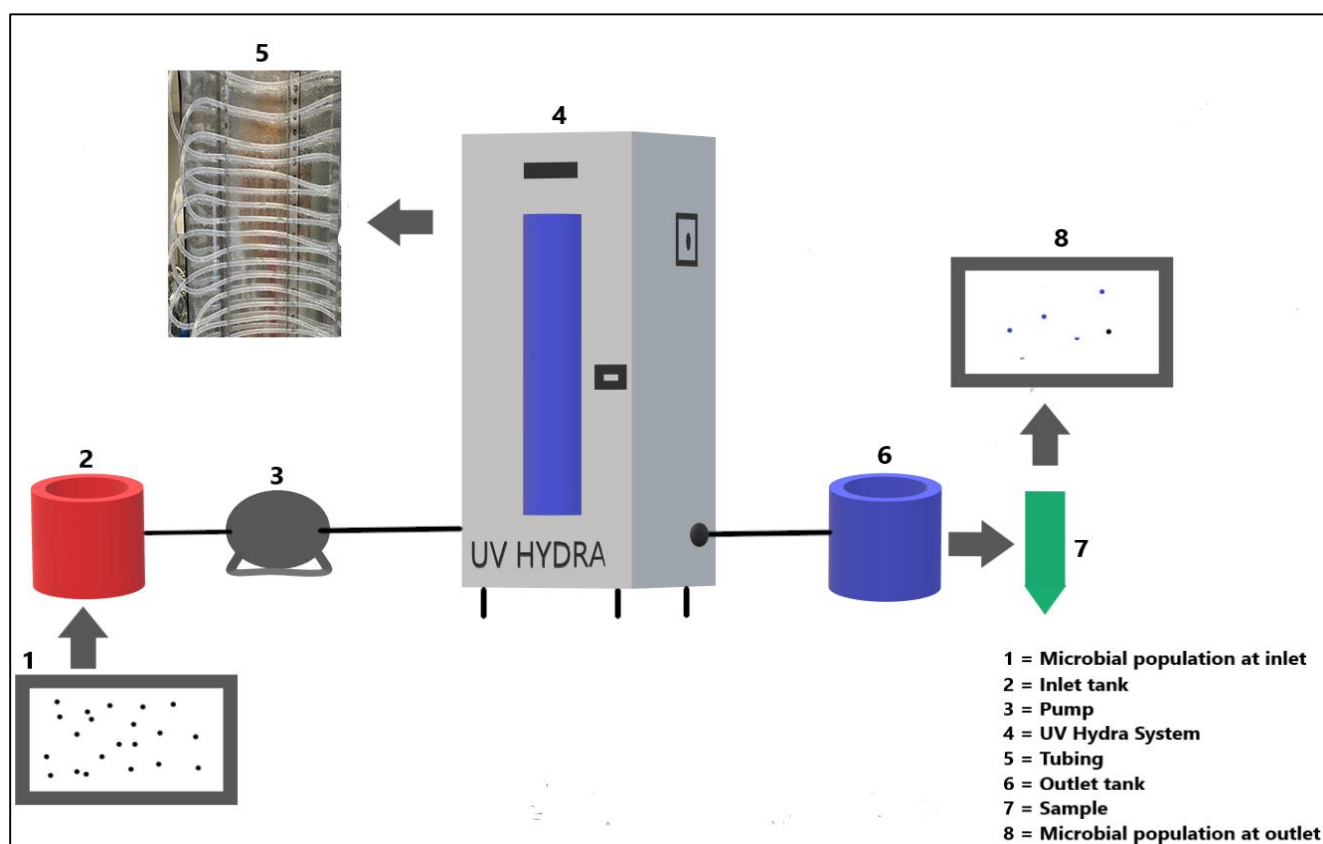
Microorganism	Flow rate (gph)	E _{EO} (kWh/m ³ /log)
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T1 UV phage	47.55	1.19 ± 0.11
<i>Bacillus cereus</i> ATCC 14579	47.55	2.67 ± 0.12
<i>Bacillus cereus</i> ATCC 14579	23.77	2.94 ± 0.05
<i>Bacillus cereus</i> ATCC 14579	11.88	3.27 ± 0.48

623 Data reported as mean ± standard deviation

624 **Figures**

625 **Fig. 1**



626

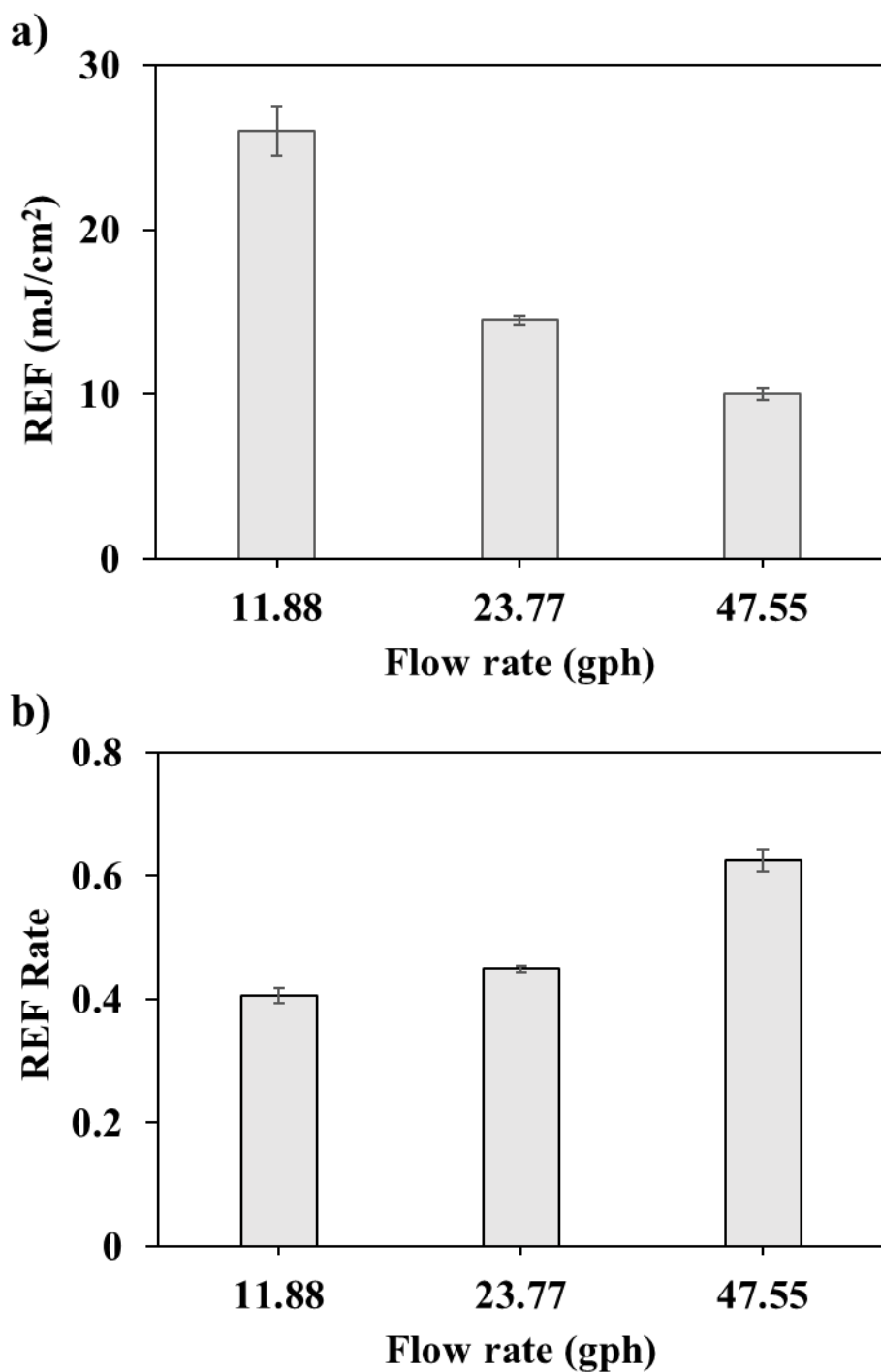
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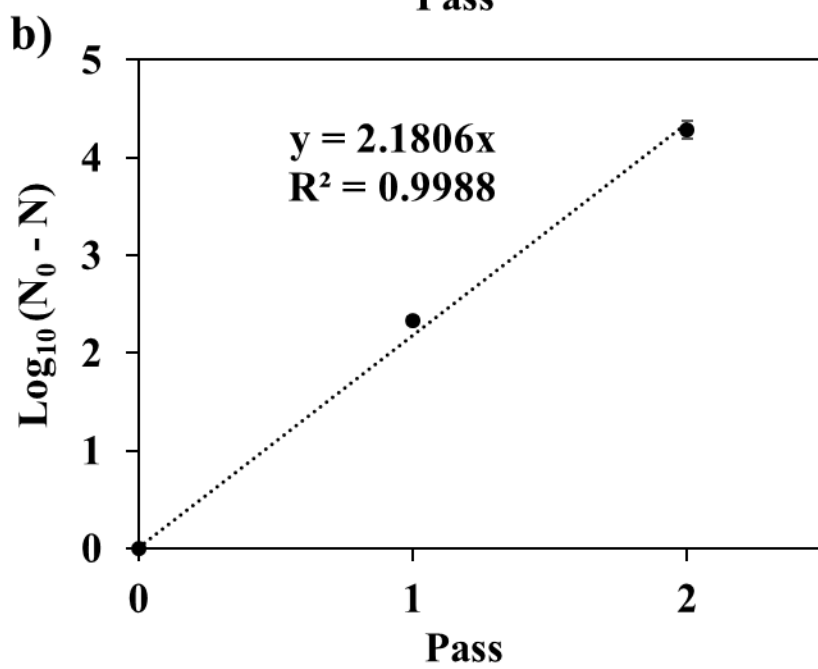
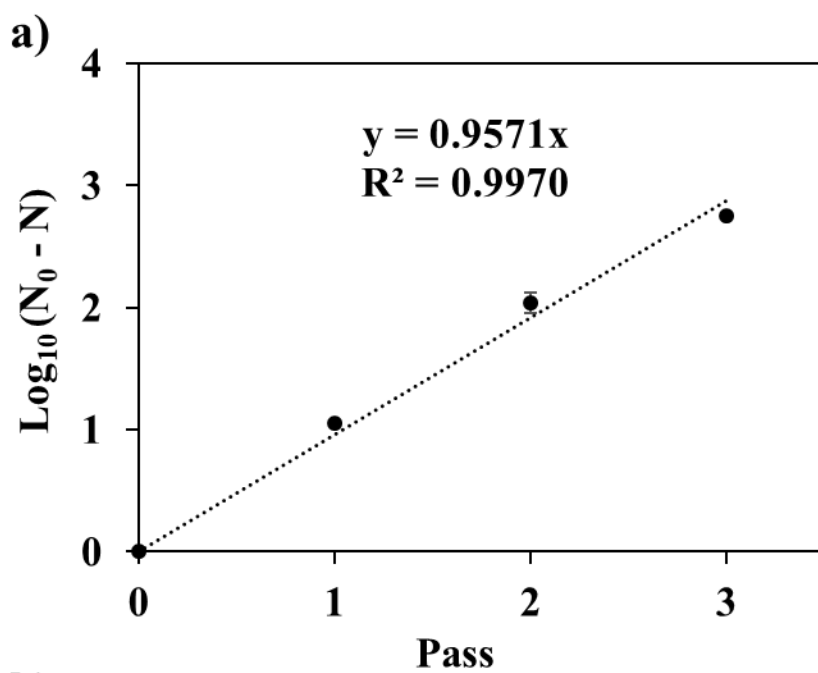
631 Fig. 2



632

633

634 **Fig. 3**

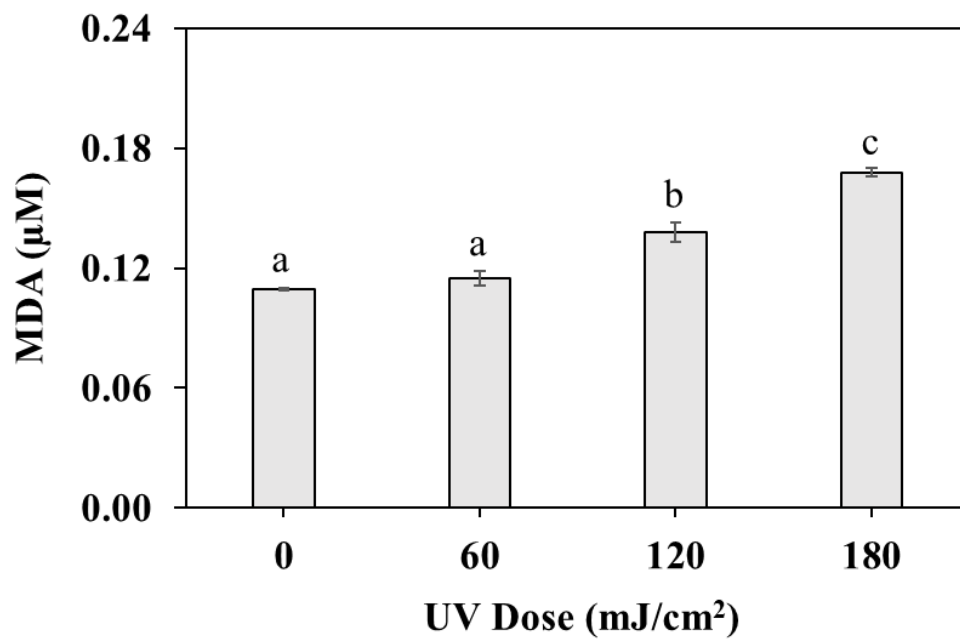


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638 **Fig. 4**



639

CRedit authorship contribution statement

Pranav Vashisht: Conceptualization, Methodology, Investigation, Visualization, Writing – original draft. **Brahmaiah Pendyala:** Conceptualization, Methodology, Investigation, Visualization, Writing – original draft, Supervision. **Ankit Patras:** Conceptualization, Methodology, Supervision, Funding acquisition. **Vybhav Vipul Sudhir Gopisetty:** Conceptualization, Methodology. **Ramasamy Ravi:** Methodology, Investigation.